

FORM PTO-1390
(REV. 6-87)U.S. DEPARTMENT OF COMMERCE
PATENT AND TRADEMARK OFFICE

ATTORNEY'S DOCKET NUMBER

09/646198

1419-00

**TRANSMITTAL LETTER TO THE UNITED STATES
DESIGNATED/ELECTED OFFICE (DO/EO/US)**INTERNATIONAL APPLICATION NO.
PCT/JP00/00199INTERNATIONAL FILING DATE
18 January 2000 (18.01.00)PRIORITY DATE CLAIMED
19 January 1999 (19.01.99)

TITLE OF INVENTION

SURFACE TREATING METHOD FOR LIGHT-METAL CASTINGS AND VEHICLE ALUMINUM WHEEL SURFACE-
TREATED BY THE SAME METHOD

APPLICANT(S) FOR DO/EO/US

Mitsuji Matsui and Atsushi Yoshida

Applicant herewith submits to the United States Designated/Elected Office (DO/EO/US) the following items under 35 U.S.C. 371:

1. ☒ This express request to immediately begin national examination procedures (35 U.S.C. 371(f)).
2. ☒ The U.S. National Fee (35 U.S.C. 371(c)(1)) and other fees as follows:

CLAIMS	(1) FOR	(2) NUMBER FILED	(3) NUMBER EXTRA	(4) RATE	(5) CALCULATIONS
TOTAL CLAIMS	19	-20=	0	x \$18.00	\$
INDEPENDENT CLAIMS	2	-3=	0	x \$78.00	
MULTIPLE DEPENDENT CLAIM(S) (if applicable)				+ \$260.00	260.00
BASIC NATIONAL FEE (37 CFR 1.492(a)(1)-(4)):					
<input type="checkbox"/> International preliminary examination fee paid to USPTO (37 CFR 1.482).....					\$750.00
<input type="checkbox"/> No international preliminary examination fee paid to USPTO (37 CFR 1.482) but international search fee paid to USPTO (37 CFR 1.445(a)(2)).....					\$760.00
<input type="checkbox"/> Neither international preliminary examination fee (37 CFR 1.482) nor international search fee (37 CFR 1.445(a)(2)) paid to USPTO.....					\$970.00
<input type="checkbox"/> International preliminary examination fee paid to USPTO (37 CFR 1.482) and all claims satisfied provisions of PCT Article 33(2) to (4).....					\$ 96.00
<input checked="" type="checkbox"/> International Search Search Report enclosed					\$840.00
Surcharge of \$_____ for furnishing the National fee or oath or declaration later than <input type="checkbox"/> 20 <input type="checkbox"/> 30 mos. from the earliest claimed priority date (37 CFR 1.482(e)).					\$130.00
TOTAL OF ABOVE CALCULATIONS					1,100.00
Reduction by 1/2 for filing by small entity, if applicable. Affidavits must be filed also. (Note 37 CFR 1.9, 1.27, 1.28.)					
SUBTOTAL					1,100.00
Processing fee of \$_____ for furnishing the English Translation later than <input type="checkbox"/> 20 <input type="checkbox"/> 30 mos. from the earliest claimed priority date (37 CFR 1.482(f)).					\$130.00
TOTAL NATIONAL FEE					1,100.00
Fee for recording the enclosed assignment (37 CFR 1.21(h)).					\$40.00
TOTAL FEES ENCLOSED					1,140.00

- a. ☒ A check in the amount of \$1,140.00 to cover the above fees is enclosed.
- b. ☐ Please charge my Deposit Account No. 13-3405 in the amount of \$_____ to cover the above fees.
A duplicate copy of this sheet is enclosed.
- c. ☒ The Commissioner is hereby authorized to charge any additional fees which may be required, or credit any overpayment to Deposit Account No. 13-3405. A duplicate copy of this sheet is enclosed.

422 Rec'd PCT/PTO 14 SEP 2000

3. A copy of the International Application as filed (35 U.S.C. 371(c)(2))
- a. ☐ is transmitted herewith (required only if not transmitted by the International Bureau).
 - b. ☐ is not required, as the application was filed in the United States Receiving Office (RO/US).
 - c. ☒ has been transmitted by the International Bureau.
4. ☒ A translation of the International Application into English (35 U.S.C. 371(c)(2)).
5. Amendments to the claims of the International Application under PCT Article 19 (35 U.S.C. 371(c)(3))
- a. ☐ are transmitted herewith (required only if not transmitted by the International Bureau).
 - b. ☐ have been transmitted by the International Bureau.
6. ☐ A translation of the amendments to the claims under PCT Article 19 (35 U.S.C. 371(c)(3)).
7. ☒ An oath or declaration of the inventor (35 U.S.C. 371(c)(4)).
8. ☐ A translation of the Annexes to the International Preliminary Examination Report under PCT Article 36 (35 U.S.C. 371(c)(5)).

Other document(s) or information included:

9. ☐ An Information Disclosure Statement under 37 C.F.R. 1.97 and 1.98.
10. ☒ An Assignment document for recording and a Recordation Form Cover Sheet - Patents Only. Please mail the recorded assignment document to the person whose signature, name and address appears at the bottom of this page.
11. The above checked items are being transmitted
- a. ☐ before the 18th month publication.
 - b. ☒ after publication and the Article 20 communication but before 20 months from the priority date.
 - c. ☐ after 20 months but before 22 months (surcharge and/or processing fee included).
 - d. ☐ after 22 months (surcharge and/or processing fee included).
- Note:** Petition to revive (37 C.F.R. 1.137(a) or (b)) is necessary if 35 U.S.C. 371 requirements submitted after 22 months and no proper demand for International Preliminary Examination was made by 19 months from the earliest claimed priority date.
- e. ☐ by 30 months and a proper demand for International Preliminary Examination was made by the 19th month from the earliest claimed priority date.
 - f. ☐ after 30 months but before 32 months and a proper demand for International Preliminary Examination was made by the 19th month from the earliest claimed priority date (surcharge and/or processing fee included).
 - g. ☐ after 32 months (surcharge and/or processing fee included).
- Note:** Petition to revive (37 C.F.R. 1.137(a) or (b)) is necessary if 35 U.S.C. 371 requirements submitted after 32 months and a proper demand for International Preliminary Examination was made by 19 months from the earliest claimed priority date.
12. At the time of transmittal, the time limit for amending claims under Article 19
- a. ☐ has expired and no amendments were made.
 - b. ☐ has not yet expired.

13. ☐ Certain requirements under 35 U.S.C. 371 were previously submitted by the applicant on _____, namely:

SCHNADER HARRISON SEGAL & LEWIS

Date: Sept. 14, 2000

By: Austin R. Miller

Austin R. Miller, Reg. No. 16,602
1600 Market Street, 36th Floor
Philadelphia, PA 19103

422 Rec'd PCT/PTO 14 SEP 2000

SPECIFICATION

SURFACE TREATMENT METHOD FOR LIGHT-METAL CAST PRODUCTS
AND VEHICLE ALUMINUM WHEEL TREATED BY THE SAME METHOD

5

TECHNICAL FIELD

The present invention relates to a surface treatment method for products cast in a light-metal material, and in particular to a surface treatment method for a light-metal cast product obtained by a die-casting process, such as a vehicle wheel made of aluminum or aluminum alloy, or especially for a high-pressure cast light-metal product, and also relates to a light-metal product treated by such a surface treatment method. The surface treatment method is suitable for forming a shiny surface having a superior metal gloss and design quality, over the whole surface or a selected surface portion of the design surface (or the casting surface) of the light metal cast product, through a casting process (hereinafter referred to as a high-pressure casting process) wherein the molten metal of aluminum or aluminum alloy (hereinafter referred to as an aluminum material) is filled in a die cavity, a pressurizing force as high as about 500 kgf/cm² to 1100 kgf/cm² (\approx 50 megapascal to 110 megapascal) in terms of metal pressure (i.e., pressure applied from the forward end of an ejection plunger to the pressure-receiving surface of the molten metal) is applied by the ejection plunger so as to perform an ejection molding, and optionally, a feeding pressure is exerted and applied to a specific portion of the molten metal during a solidification step thereof by using a pressurizing pin (or a squeeze pin) installed on a die.

PRIOR ART

A cast product made of a light metal material, especially of an aluminum material, such as an aluminum wheel, is a high strength component, and also is a

commodity requiring gloss and a design quality. In the case of a vehicle wheel, many users currently tend towards a preference for an aluminum material having a metal gloss on a design surface. On the other hand, a cast product of an aluminum material is normally cast by a medium or low-pressure casting process using a pressure range (about 0.01 megapascal to 0.050 megapascal, for the low-pressure casting process) lower than the pressure used in the high-pressure casting process described above, which results in many pinholes, some of which are large and form deep recesses. Various surface treatment methods for treating the cast aluminum wheel to produce a shiny surface have been studied, and typically, the following three methods are adopted:

(a) a method in which the casting surface forming the design surface of the cast aluminum wheel is polished by a buffing process, or is buffed and thereafter coated with a transparent coat;

(b) a method in which the casting surface forming the design surface of the cast aluminum wheel is polished and coated with wet-type nickel and chromium platings;

(c) a method in which the casting surface forming the design surface of the cast aluminum wheel is coated with a resin coating layer, and a dry-type plating layer is formed thereon and thereafter coated with a transparent coat.

Among these methods, the method (a) poses the problem that it is difficult to buff the recesses in the casting surface. Consequently, small openings remain unfilled in the design surface. Especially, in the case of a wheel having a design difficult to buff, a sufficient shine may not be achieved.

In method (b), on the other hand, large pinholes, if any, cause insufficient adherence of the chrome plating on the surface which has been polished by a mechanical grinding but has not been machined or was insufficiently machined. These portions easily develop separation of or

corrosion under the plating layer. In order to improve these points, many methods for producing a surface capable of being plated with chromium are used in current general plating processes, wherein, as described in, 5 e.g., Japanese Unexamined Patent Publications (Kokai) No. 6-293974 and 6-2939993, the design surface of a cast aluminum wheel is treated, as a chromate treatment, with chromic acid or shot-blasting so as to close the pinholes formed in the cast aluminum wheel. In this case, 10 however, recycling of the wheel may be difficult. Specifically, in the case where a recycle dealer is entrusted to recycle the plated wheel, separation of chromium or nickel from an aluminum alloy is very expensive. Also in the case where the aluminum wheel is 15 melted in a factory, a large amount of nickel and chromium plated on the surface thereof are mixed with the aluminum alloy as impurities. It is impossible, therefore, to melt the plated wheel products alone. So, it is required to perform the melting process together 20 with an ingot (which contains nickel and chromium at not more than a specified amount). This poses another problem that a many wheels cannot be recycled at one time.

For the reasons mentioned above, the method (c) has 25 been developed and was recently commercialized. The known technique relating to the method (c) is described in Japanese Examined Patent Publication (Kokoku) No. 6-73937. According to this technique, the surface treatment is accomplished as follows:

30 (1) the surface of a metal material is shot-blasted and thereafter is coated with a powder to provide a primer coat;

(2) a transparent undercoat is applied as an intermediate layer on the powder coating;

35 (3) chromium is sputtered on the undercoat;

(4) a transparent top coat is applied on the sputtering layer.

This method is superior in that a shiny surface can be obtained without the polishing process which is indispensable for the methods (a) and (b).

On the other hand, to obtain a design surface having a metal gloss superior in design quality, the roughness of the shot-blasted surface must be smoothed out by powder coating. The shot-blasting process forms an unevenness, at least on the order of several tens of μm , on the surface of material. Therefore, the powder coating having the thickness of at least 100 μm is required to smooth the unevenness. Especially in the case where the surface gloss is important and it is required to completely eliminate the unevenness on the surface after powder coating, a thickness of not less than 150 μm is required.

In another surface treatment method, disclosed in Japanese Unexamined Patent Publication (Kokai) No. 6-227201, the design surface, of an aluminum wheel obtained by casting, is treated by a primer coat, thereafter is sputtered with aluminum, and the surface thereof is protected by a transparent coat. In this way, the aforementioned disadvantage which otherwise might result from the dry-type plating layer is obviated.

However, pinholes cannot be completely closed up, even by the method disclosed in the Kokai No. 6-227201. Consequently, the gas contained in the pinholes may expand or break the coating during a baking finish process of the prime coat wherein the temperature of the aluminum wheel is increased about 150°C , which causes a problem in that pits are formed on the surface of the sputtering layer and thereby a satisfactory design quality cannot be produced.

On the other hand, the technique disclosed in Japanese Unexamined Patent Publication (Kokai) No. 9-290213 is constituted as described below. First, the surface of the metal material is degreased and washed in

water. Then, at least one layer of "a colored base coat" and "a colored or transparent resin" is applied. The surface thereof is covered with "a sputtering film", and a transparent "top coat" is applied thereon. In the
5 embodiment disclosed in the Kokai No. 9-290213, the thickness of the "colored base coat" is 10 to 30 μm , and a powder coating layer of 60 to 150 μm is applied thereon. Therefore, the thickness of the prime layer including the "sputtering film" is about 70 to 180 μm .

10 However, the powder coating, being thicker than the normal thickness, applied before the dry-type plating process has posed problems as follows:

•the thicker the prime resin layer for leveling to remove the unevenness caused in the shot-blasting
15 process, the larger the deterioration of an antichipping characteristic, so that a satisfactory result cannot be obtained in an acceptability determining test conducted by a predetermined method;

•the cost is increased due to the thicker powder
20 coating;

•even if a very hard dry-type plating is applied, a high surface hardness cannot be provided as the thickness of the resin layer increases, because the resin layer constituting the prime coat of the dry-type
25 plating is so soft that the thicker the resin layer, the more significantly the surface hardness is affected.

In recent aluminum wheels for vehicles, to meet the demand for an improved strength, by increasing the internal density of the casting, the die casting is
30 sometimes conducted, for forming a cast product of an aluminum material, by setting the casting pressure in a high range rather than in a low or middle range. In the case of the aluminum wheel formed under a pressurizing force in such a high range, however, a release agent
35 coated on the die may not be sufficiently removed from the surface of the metal material by "the degreasing and

washing in water" after the casting process. In other words, the release agent tends to be strongly attached to the surface of the metal material during the casting process, and thus cannot be easily removed.

On the other hand, even when the casting pressure is set to a high pressure range, it is generally considered difficult to completely eliminate the generation of pinholes from the surface of the cast aluminum product. In order to remove the release agent and to close the remaining pinholes, the surface of the material is usually cleaned by use of a comparatively inexpensive shot-blasting process. Specifically, in order to conduct the surface treatment of cast aluminum products formed in high pressure range by the method described in the Kokai No. 9-290213, the shot-blasting process is executed. Therefore, even in the casting process in the high pressure range, the thickness of the prime layer of the sputter film is required to be not less than 100 μm , or in some cases, not less than 150 μm . This unavoidably deteriorates the chipping characteristic as described above, and the cast product cannot pass a final test for determining the acceptability.

DISCLOSURE OF THE INVENTION

In view of the above-mentioned problems of the prior art, the main object of the present invention is to provide a surface treatment method, for a light-metal casting, in which the internal strength and the casting surface of an aluminum casting have predetermined high qualities, before the surface treatment is conducted, by selecting the casting condition of the light-metal material, especially of the aluminum material, so that the subsequent surface treatment step can produce a shiny surface superior in metal gloss and design quality and a superior chipping characteristic, and also to provide an aluminum cast product subjected to such a surface treatment method.

Another object of the invention is to provide a surface treatment method for a light-metal cast product, obtained by a high-pressure casting process from a light-metal material such as an aluminum material, on which a dry-type plating is coated so as to produce a metal gloss, wherein the thickness of the priming resin under the dry-type plating film is reduced to a range between 10 μm and 40 μm , which is thinner than the conventional priming resin, and thereby realizing a metal gloss superior in design quality.

Still another object of the invention is to provide a surface treatment method and an aluminum cast product, especially an aluminum wheel, subjected to the surface treatment method, wherein the casting surface of the light-metal casting, which is obtained through a high-pressure casting process capable of remarkably reducing the number and size of pinholes generated during the casting process, is subjected to a direct polishing process so as to remove the pinholes on the casting surface to form a smooth polished surface, without performing shot-blasting or a chromate treatment with chromic acid, so that a uniform and thin resin coating layer is attached as an undercoat, and wherein a dry-type plating layer of the desired metal such as aluminum is formed to produce a design surface superior in shininess and gloss and capable of passing an acceptability determination test for a chipping characteristic conducted according to a predetermined procedure.

In order to achieve the above objects, the present invention adopts a polishing process, especially, a barrel finishing process on the casting surface of a light-metal casting, in place of the conventional shot-blasting process. After the barrel finishing process, the first resin coating is applied as a primer of a dry-type plating. The barrel finishing is a method of polishing in a dry condition by using a mixture, called a medium, of a powder material and an abrasive. After the

barrel finishing process, the first resin coating layer having a thickness not less than 10 μm and not more than 40 μm is formed on the polished surface, and further a dry-type plating layer is formed on the surface of the first resin coating layer. The dry-type plating is for forming a predetermined metal coating layer by a sputtering process, and, in the case where the dry-type plating layer is soft, a topcoat layer is formed of a transparent second resin coating on the dry-type plating layer.

The applicable polishing process can include a buff polishing process or a liquid honing process, instead of the barrel finishing process. The buff polishing process is one in which an abrasive is held in a buff made of a soft material such as a cloth and the buff is rotated while being abutted against a workpiece to polish it. The abrasive used in this process is fixed by an adhesive on the outer peripheral surface of the buff or is mixed with a medium such as water to be sprayed on the buff. The liquid honing process is a method in which a polishing liquid is injected from a nozzle to a workpiece to polish it. The polishing liquid is generally a mixture of water and alumina or white alundum, etc. The barrel finishing process has the advantage, as compared with the buff polishing process, that the polishing process can be completed within a shorter time and mass treatment can be performed to reduce a polishing cost. Also, as compared with the liquid honing process, a mirror polished surface can be advantageously obtained and the thickness of the prime resin for smoothing the polishing surface can be advantageously reduced.

In the case of a casting produced by a low-pressure casting method or a weight casting method, the application of the resin coating to the barrel-polished surface makes parts of the coating surface bubble as small as a sesame seed or an azuki bean. These bulges

are generated as the gas in the many pinholes on the polished surface is expanded by the heat treatment during the painting process. In the conventional shot-blasting process, many pinholes are crushed by shot particles colliding under high pressure, and therefore the problem of bulges rarely occurs. In the barrel finishing process, however, most pinholes remain uncrushed.

The dry-type plating on the coating surface may also pose a problem. Specifically, an attempt to increase the vacuum degree in a chamber accommodating a casting for a dry-type plating often fails as gas in the pinholes leaks out through the resin coating film. The thin resin coating according to this invention further facilitates the passage of the gas through the resin coating film and a longer time is required before the vacuum degree is increased.

Therefore, it is readily comprehended that, in an aluminum wheel cast by the low-pressure casting process, a metal gloss superior in design quality cannot be easily obtained by "applying the resin coating after barrel polishing and also applying the dry-type plating thereon".

The present inventors have discovered that a high-pressure casting process can sufficiently reduce the number of pinholes and the dimension of the opening of the latter (i.e., a pinhole size) on the casting surface, and that the above-described surface treatment method can be successfully accomplished. It has also been found that a casting surface having a metal gloss superior in design quality can be obtained by performing the above-described surface treatment method on the casting obtained by the high-pressure casting process as already described. In the case where the pressure cannot be easily transmitted under such conditions that "the sectional area of the gate is small", however, the pressure of the ejection plunger fails to be sufficiently transmitted to the casting surface far from the gate, and

pinholes still remain unclosed. Therefore, it is difficult to obtain a surface having a metal gloss superior in design quality.

In view of this, the present inventors have
5 conducted a casting test "under such a die condition for an aluminum wheel that a pressurizing pin is arranged in opposed relation to a die gate to pressurize simultaneously with a solidification and contraction".
As a result, it was found that the pressure is
10 sufficiently transmitted to the design surface of the casting so that the above surface treatment method can produce a metal gloss superior in design quality. Thus the problem mentioned above was solved.

According to the present invention, there is
15 provided a surface treatment method for a light-metal casting, comprising:

a casting step for applying a casting pressure of more than about 50 megapascal from an ejection plunger to a molten metal of a light-metal material poured into a
20 die, to form a casting having pinholes generated in a casting surface, the pinholes being suppressed so as to meet a predetermined condition;

a polishing step for reducing a surface roughness of a polished surface obtained by polishing the
25 casting surface to not more than a predetermined value;

a painting step of forming a first resin coating layer on the polished surface; and

a plating step for forming a layer of a metal or a metal compound through a dry-type plating on a
30 surface of the resin coating layer.

Preferably, the predetermined condition of the pinholes generated on the polished surface is that the number and a maximum opening dimension of the pinholes generated in a predetermined area of the polished surface
35 is not more than a predetermined value. Especially, it is preferred that the number of the pinholes is 1 to 15 per 100 cm² of the polished surface and the maximum

opening dimension is not more than 2 mm. More preferably, the number of the pinholes is in the range of 1 to 10 per 100 cm² of the polished surface, the maximum opening dimension is not more than 2 mm and the number of the pinholes having the maximum opening dimension of 1.0 to 2.0 mm is one or zero.

Preferably, the surface roughness of the polished surface obtained by the polishing process is 6.3 μm in Rmax.

Preferably, the thickness of the first resin coating layer is not less than 10 μm and not more than 40 μm, and a transparent second resin coating layer is formed as a top coat layer on the dry-type plating layer of a metal or a metal compound.

Preferably, the casting step includes a pressurizing step for applying a squeeze pressure by a pressurizing pin to a predetermined portion of the molten metal of the light-metal material filled in a die cavity during a solidification process of the molten metal under a high pressure.

According to this invention, there is provided a shiny aluminum vehicle wheel, characterized in that the aluminum wheel is cast by a high-pressure casting process, in which a molten metal of an aluminum material filled in the cavity of a vehicle wheel casting die is pressurized by an ejection plunger and, in a solidification process of the molten metal, a portion of the molten metal corresponding to a formed wheel boss is pressurized by a pressurizing pin arranged in the die, so that pinholes generated in a casting surface of an aluminum casting have a dimension of not more than 1.0 mm diameter and the number is not more than 10 per 100 cm² area; and that the aluminum wheel comprises a structure wherein the casting surface is a barrel-polished surface with a roughness Rmax of not more than 1.6 μm, a resin coating layer with a thickness of not less than 10 μm and

not more than 40 μm is formed as an undercoat on the barrel-polished surface, a dry-type plating layer made of a metal or a metal compound is formed on the resin coating layer and a transparent topcoat layer is formed on the dry-type plating layer so as to provide a design surface.

In the surface treatment method for the light-metal casting having the aforementioned structure, an aluminum wheel made by a high-pressure casting process is polished so that the surface of the aluminum wheel is polished almost to a mirror-surface although slight polishing scars remain thereon. Thus, the mirror-surface treatment of the aluminum wheel surface is made possible by forming a resin coating layer thinner than that in the shot-blasting process. Especially, the barrel finishing process can provide a mirror surface of the aluminum wheel with a resin coating layer as thin as not less than 10 μm and not more than 40 μm , which is remarkably thinner than that in the shot-blasting process.

BRIEF DESCRIPTION OF THE DRAWINGS

The above and other objects, features and advantages of this invention will be made apparent by the description taken in conjunction with the accompanying drawings, in which:

Fig. 1 is a flowchart illustrating a cast body producing process and a surface treatment process for a light-metal cast product according to an embodiment of the present invention;

Fig. 2 is a sectional view of essential parts, schematically showing a construction of a high pressure casting apparatus for casting a light-metal casting under a high pressure;

Fig. 3 is a sectional view schematically showing a high pressure casting apparatus wherein a pressurizing pin operating mechanism is omitted, as a modification of the high pressure casting apparatus shown in Fig. 2;

Fig. 4 is a sectional view schematically showing a construction of a barrel finishing machine used for carrying out the surface treatment method according to this invention;

5 Fig. 5 is a sectional view showing an example structure of an aluminum wheel which is cast by the high pressure casting method and treated by the surface treatment method according to the invention;

10 Fig. 6A is an enlarged sectional view showing the surface treated state of portion "A" of the aluminum wheel shown in Fig. 5;

Fig. 6B is an enlarged section view similar to Fig. 6A, showing a light-metal cast product treated by a conventional surface treatment method;

15 Fig. 7 is a perspective view schematically showing a construction of a test device for testing the antichipping performance of a light-metal cast product subjected to a surface treatment;

20 Fig. 8 is a diagram showing a part of the surface portion indicating the result of an antichipping performance test conducted after a cast aluminum wheel made by the conventional middle or low pressure casting method is treated by the conventional surface treatment method; and

25 Fig. 9 is a diagram showing a part of the surface portion indicating the result of an antichipping performance test conducted on an aluminum wheel which is cast by the high pressure casting method and treated by the surface treatment method according to this invention.

30 BEST MODE FOR CARRYING OUT THE INVENTION

Now, specific embodiments of the invention will be explained in detail with reference to the accompanying drawings.

35 Referring to the flowchart of Fig. 1 illustrating the process of high pressure casting and surface treatment, according to this invention, an aluminum wheel is first cast by the high pressure casting process (step

00445130 "004400
00445130 "004400

100). In this process, a molten metal of an aluminum material is filled in a cavity 14 of a die 12 through an ejection plunger 16 by using a high pressure casting apparatus 10 as shown in Fig. 2, and a high pressure of about 50 megapascal to 110 megapascal is applied to the molten metal in the cavity 14 from the front end surface of the ejection plunger 16. A most preferable embodiment comprises a pressurizing pin 20 in opposed relation to a gate 18 of the die 12. In the solidification process of the molten metal, simultaneously with the pressurizing step of the molten metal filled in the die cavity 14 by the ejection plunger 16, the pressurizing pin 20 pressurizes, due to the operation of a hydraulic cylinder 22, a portion of the molten metal opposed to the gate 18. As a result, the pressure of the ejection plunger 16 is sufficiently transmitted to a casting surface area far from the gate 18. Thus, pinholes can be prevented from existing in the casting surface after the casting process is completed, and a density improvement after solidification can be facilitated. The operation of the pressurizing pin 20 may be controlled in such a manner as to apply a pressurizing force in accordance with a desired pressure curve (i.e., a curve of time vs. pressure) from an optimum timing by a changeover four-way valve 24. Because the generation of pinholes on the casting surface can be sufficiently reduced by the above described high pressure casting process as compared with the low-pressure or medium-pressure casting process, without operating the pressurizing pin 20, it can be seen that the functions and effects of the present invention can be achieved by the surface treatment method, described below, performed on a light-metal casting, such as an aluminum material, cast through a high pressure casting apparatus (see Fig. 3) with no pressure pin 20. Referring again to the flowchart of Fig. 1, the aluminum wheel cast body removed from the die 12, after the high pressure casting is completed, is treated in a desired

heat treatment step (step 105), and a machining step, such as a machining of the rim thereof, is performed in accordance with the dimensions and profile of a vehicle wheel (step 106). The aluminum wheel cast body thus
5 subjected to the machining step is designated by, e.g. a reference numeral 26 in Fig. 4, and the casting surface thereof is then subjected to a barrel finishing step as shown in Fig. 4 (step 110).

In the barrel finishing step, the aluminum wheel
10 cast body 26 is mounted on the barrel finishing machine 28. First, medium 30 comprising a mixture of corn or cork and abrasives is charged into a barrel bath 32. The aluminum wheel cast body 26 fixed on a disk connected to a motor shaft is inserted into the medium 30 in the
15 barrel bath 32. In this condition, a motor M1 is started, and the rotational motion indicated by an arrow is transmitted through the disk 34, so that the aluminum wheel cast body 26 rotates in the medium 30 and the medium 30 collides with the surface of the aluminum wheel
20 cast body 26, so as to polish the casting surface of the cast body 26 into a fine surface condition. In the barrel finishing step, a motor M2 is used in the case where the aluminum wheel cast body 26 is to be lowered and positioned within the abrasive in the barrel bath 32.

25 The aluminum wheel cast body 26, after passing through the barrel finishing step, is taken out from the barrel bath 32 of the barrel finishing machine 28, and is cleaned and degreased through a degreasing step by an appropriate cleaning agent such as water (step 112).

30 Further, the cast body is subjected to the normal chromate treatment for improving the adhesiveness between the casting surface and the coating layer (step 114).

The aluminum wheel cast body 26, after the chromate treatment is completed, is dried in a drying step (step
35 116), and thereafter is subjected to a primer coating step using resin paint, i.e. an undercoating step (step 120). In this undercoating step, an overlapped coating

layer is preferably formed by the primer coating and the solvent type coating. The primer coating improves a corrosion resistance by using, e.g., an epoxy type resin paint, while the solvent coating improves the adhesiveness of the subsequent dry-type plating by using a polyester type paint and a melamine type solvent paint. In this way, a resin coating layer is formed on the casting surface after being subjected to the barrel finishing, and thereafter the coating layer is baked at 160 °C to 180 °C for 20 minutes (step 130). The thickness of this resin coating layer is selected to be not less than 10 μm and not more than 40 μm.

After the undercoating step, using a resin paint, is completed, the dry-type plating step is effected on the upper surface of the undercoating layer (step 140). As the dry-type plating, three type methods such as sputtering, vacuum evaporation and ion plating are known. Among them, sputtering is most suitably used, because it is superior in film-forming property even for a complicated shape of the design surface of the vehicle aluminum wheel. As the sputtering film, an aluminum film or the like having the thickness of 0.1 μm to 1.0 μm is formed. In the case where a topcoat layer is formed on the sputtering film (step 150), a paint of a urethane type, an acryl type or an epoxy type resin is used and the coating is set to a thickness of about 25 μm to 30 μm. The topcoat layer may be made by using a transparent powder.

The paint of the topcoat layer formed in the manner described above is baked at 100 °C to 160 °C for 20 minutes (step 160).

According to this embodiment, the prime resin coat under the dry-type plating film can have a thickness not less than 10 μm and not more than 40 μm, which is much thinner than the conventional thickness, and an aluminum

wheel product can be finally obtained through a surface treatment for producing a metal gloss superior in design quality.

Fig. 5 is a sectional view showing an aluminum wheel 26a cast by the high pressure casting process and obtained through the surface treatment process described above, which includes a wheel rim 40 on which a tire 50 is mounted, and a wheel hub 42 having, e.g., a central hub hole permitting it to be coupled to a vehicle axle. It should be understood that the sectional shape of the aluminum wheel 42, or especially the sectional shape of the wheel hub 42 is varied from one to another taking the design quality and the strength thereof into consideration, and the shown one is only an example.

Fig. 6A shows and picks out the portion A of the aluminum wheel 26a and is an enlarged view of the surface treatment structure of the design surface of the wheel hub 42. Fig. 6B is a sectional view showing, for comparison with Fig. 6A, a similar aluminum wheel cast body subjected to the surface treatment using a conventional surface treatment method, which cast body is cast by a conventional low-pressure casting method (a molten metal is poured into a die by an application of a low pressure of 0.050 megapascal (about 0.5 kg/cm²) on the surface of the molten metal).

As is clear from the comparison of the surface treatment structures shown in Figs. 6A and 6B, according to the invention shown in Fig. 6A, because the aluminum wheel cast body 26a is cast by the high pressure casting process, and therefore the casting surface is essentially formed as a smooth surface having a sufficiently reduced number of pinholes, the casting surface can be further buffed or otherwise processed into a still smoother casting surface, and an undercoat layer, a dry-type plating layer and a topcoat layer can be formed in this order by the surface treatment method and, consequently, a design surface of high quality which exhibits the

shininess of a metal film formed as a dry-type plating layer by the sputtering or the like, without unduly increasing the entire thickness of a surface treated layer, can be obtained. In the example shown in Fig. 6A, the topcoat layer is formed of a primer coating and a solvent coating as a preferable typical example. Alternatively, it should be understood that the topcoat layer can be formed of a transparent powder.

In the prior art shown in Fig. 6B, on the other hand, the casting surface of a cast body of an aluminum material formed by the low-pressure casting method is subjected to the shot blasting to close up the pinholes, a thick prime coating layer (with a polyester type powder coating) is formed on the shot-blasted surface to remove the unevenness of the casting surface caused by the shot blasting, an aluminum material film is formed on the smooth surface of the polyester/melamine type solvent coating layer, and an acryl-silicon type solvent coating is applied as a topcoat layer. This construction has a large entire thickness of the surface treated layers, resulting in a deteriorated antichipping performance as described later.

Fig. 7 schematically shows a construction of a test mechanism for conducting an antichipping performance test conventionally used for a quality evaluation test of the design surface of a cast product, especially, a vehicle aluminum wheel, subjected to a required surface treatment on the casting surface of a cast body made of a light-metal material such as aluminum. As shown in Fig. 7, a test piece 60 is arranged above an appropriate screen 70 or on the surface of the screen. A predetermined amount of stones having a predetermined size is injected from a predetermined position by a pressurized air flow in a direction perpendicular to the surface 60A to be tested of the test piece 60, so that the quality of the design surface is evaluated on the basis of the dimension and number of various defects or recesses formed on the

tested surface 60A.

In Fig. 7, a predetermined amount of stones are introduced into a funnel 64 as shown by an arrow S, and an air flow is introduced in predetermined pressure as shown by an arrow R, thereby the injection is performed from an injection pipe 66 as shown by an arrow T. This antichipping performance test is based on the standards of American Society for Testing Materials (ASTMD3170), wherein the acceptability of the quality is determined by visually comparing the defects formed on the tested surface 60A with a certain standard sample surface prepared in advance.

As a condition for the antichipping performance test for a typical vehicle aluminum wheel, basalt No. 6 (4.8 mm to 8.0 mm in diameter) is used as the stones, and the test is conducted by using about 100 grams of the stones at the injection rate of 50 g/sec, the ejection pressure of 4.1 kg/cm² (about 0.402 megapascal), with the distance from the test surface being set at 35 cm. In conducting the test, Fly Rock Tester (Model: JA400) made by Suga Shikenki KK (Suita City, Osaka) is used, which is a typical testing device based on the operating principle shown in Fig. 7.

Figs. 8 and 9 show the result of the antichipping performance tests conducted respectively on the design surfaces of the vehicle aluminum wheel produced through the low-pressure casting method and the surface treatment method according to the prior art and of the vehicle aluminum wheel produced by the high-pressure casting method and the surface treatment method according to the invention. It is seen that the wheel of the prior art shown in Fig. 8 has larger chipping defects and a larger number of chipping defects.

In contrast, in the aluminum wheel to be tested according to the invention shown in Fig. 9, it can be seen that the number of chipping defects is remarkably reduced and the dimension of chipping defects is smaller.

In other words, the chipping characteristics of the wheel design surface according to the invention appear to be far superior to that of the prior art.

Referring now to Table 1, the condition of pinholes which remain per 100 cm² in portions B1 to B3 on the casting surface (i.e., the casting surface portions corresponding to the wheel portions indicated by arrows B1 to B3 of the aluminum wheel 26A shown in Fig. 5) is listed, wherein two sample cast bodies including a vehicle aluminum wheel cast by the high-pressure casting method with a pressurizing pin according to the invention and a vehicle aluminum wheel cast by the high-pressure casting method alone, and an aluminum wheel cast by the low-pressure casting method according to the prior art, are subjected to the barrel finishing process shown as step 110 in Fig. 1, whereby the respective wheel casting surfaces are finished into one of three removed-material thickness ranges of 40 to 60 μm, of 140 to 160 μm and of 280 to 300 μm.

From Table 1, it is seen that, at each of the portions B1, B2 and B3, the two sample aluminum wheels cast by use of the high-pressure casting process according to the invention (i.e., the high-pressure casting with a pressure pin or the high-pressure casting alone) have a much smaller number of pinholes at all portions on the polished surface than the sample aluminum wheel cast by the conventional low-pressure casting method. Especially, the number of pinholes with large opening dimensions of 1.0 to 2.0 mm diameter appears to be reduced remarkably. Specifically, with the increase in the removed thickness, the high-pressure casting method with squeeze pressure being imparted by the pressure pin appears to form only 15 or less residual pinholes per 100 cm² at any wheel portion and a very small number of residual pinholes with large opening dimensions. Accordingly, by treating the high-pressure

cast body of an aluminum material having such a small number of generated pinholes and a small number of large pinholes with the surface treatment process shown in steps 105 to 160 of Fig. 1, a wheel design surface having a very superior antichipping performance, as shown in Fig. 9, can be obtained.

On the other hand, the sample aluminum wheel produced by the low-pressure casting method according to the prior art appears to have a large number of generated pinholes and a large number of larger pinholes, both remaining in the polished surface, even when the removed thickness by barrel finishing is increased. As a result, an aluminum wheel produced by the low-pressure casting method essentially requires crushing of the pinholes by shot-blasting. It is therefore necessary to increase the thickness of the undercoat and to level the undercoat layer on which the metal plating layer is sputtered. This unavoidably deteriorates the antichipping performance of the design surface, as shown in Fig. 8, in the case where a coating layer is superposed as a topcoat layer on the metal plating layer or the like.

As a method of evaluating the coating quality of the design surface of the surface-treated aluminum wheel, various testing methods such as a corrosion resistance test, a weather resistance test, and so on, are generally used and are well known, in addition to the antichipping performance test described above. It has been ascertained that the design surface of a light-metal cast body produced by the surface treatment method according to the invention passes the test provided by the aforementioned evaluation methods.

It will be easily understood by those skilled in the art that the objects, on which the surface treatment method according to the invention is applied, are not limited to an aluminum wheel, but are applicable to other cast bodies of a light-metal material produced through a high-pressure casting process.

Table 1 Condition of pinholes in finished surface

Casting process	Portions	Removed thickness by barrel finishing		
		40 - 60 μ m	140 - 160 μ m	200 - 300 μ m
High-pressure casting + Pressurizing pin	B1	$\phi 0.5$ or less: 5 pieces	$\phi 0.5$ or less: 3 pieces	$\phi 0.5$ or less: 2 pieces $\phi 0.5 - 1.0$: 1 piece
	B2	$\phi 0.5$ or less: 4 pieces $\phi 0.5 - 1.0$: 4 pieces	$\phi 0.5$ or less: 3 pieces $\phi 0.5 - 1.0$: 1 piece	$\phi 0.5$ or less: 5 pieces
	B3	$\phi 0.5$ or less: 9 pieces $\phi 0.5 - 1.0$: 2 pieces	$\phi 0.5$ or less: 6 pieces $\phi 0.5 - 1.0$: 3 pieces	$\phi 0.5$ or less: 3 pieces $\phi 0.5 - 1.0$: 2 pieces
	B1	$\phi 0.5$ or less: 4 pieces	$\phi 0.5$ or less: 2 pieces $\phi 0.5 - 1.0$: 2 pieces	$\phi 0.5$ or less: 2 pieces
High-pressure casting	B2	$\phi 0.5$ or less: 7 pieces $\phi 0.5 - 1.0$: 6 pieces	$\phi 0.5$ or less: 5 pieces $\phi 0.5 - 1.0$: 5 pieces	$\phi 0.5$ or less: 3 pieces $\phi 0.5 - 1.0$: 3 pieces
	B3	$\phi 0.5$ or less: 5 pieces $\phi 0.5 - 1.0$: 2 pieces $\phi 1.0 - 2.0$: 1 piece $\phi 2.0$ or more: 1 piece	$\phi 0.5$ or less: 8 pieces $\phi 0.5 - 1.0$: 6 pieces	$\phi 0.5$ or less: 4 pieces $\phi 1.0 - 2.0$: 1 piece
	B1	$\phi 0.5 - 1.0$: 2 pieces $\phi 1.0 - 2.0$: 1 piece $\phi 2.0$ or more: 3 pieces	$\phi 0.5$ or less: 5 pieces $\phi 0.5 - 1.0$: 2 pieces $\phi 2.0$ or more: 2 pieces	$\phi 0.5$ or less: 2 pieces $\phi 0.5 - 1.0$: 6 pieces $\phi 1.0 - 2.0$: 1 piece
	B2	$\phi 0.5$ or less: 5 pieces $\phi 0.5 - 1.0$: 2 pieces $\phi 1.0 - 2.0$: 1 piece $\phi 2.0$ or more: 6 pieces	$\phi 0.5$ or less: 3 pieces $\phi 0.5 - 1.0$: 12 pieces $\phi 2.0$ or more: 1 piece	$\phi 0.5$ or less: 6 pieces $\phi 1.0 - 2.0$: 1 piece $\phi 2.0$ or more: 2 pieces
Low-pressure casting	B3	$\phi 0.5$ or less: 9 pieces $\phi 0.5 - 1.0$: 2 pieces $\phi 1.0 - 2.0$: 1 piece $\phi 2.0$ or more: 4 pieces	$\phi 0.5$ or less: 5 pieces $\phi 0.5 - 1.0$: 6 pieces $\phi 2.0$ or more: 3 pieces	$\phi 0.5$ or less: 4 pieces $\phi 0.5 - 1.0$: 7 pieces $\phi 1.0 - 2.0$: 1 piece $\phi 2.0$ or more: 5 pieces

As is apparent from the foregoing description, according to this invention, barrel finishing is carried out on the surface of an aluminum wheel before applying a resin coating of a solvent type as a priming step of a dry-type plating process on the surface of a light-metal material such as an aluminum wheel. Compared with the prior art in which a powder coating layer of not less than 100 μm or in some cases not less than 150 μm is required, the surface can be sufficiently smoothed simply by attaching a resin coating layer of a solvent type in the thickness range of not less than 10 μm and not more than 40 μm , thereby leading to a great advantage that a design surface superior in design properties and antichipping performance, and having a metal gloss, can be obtained at low cost.

CLAIMS

1. A surface treatment method for a light-metal casting, characterized by comprising:

5 a casting step for applying a casting pressure of more than about 50 megapascal from an ejection plunger to a molten metal of a light-metal material poured into a die, to form a casting having pinholes generated in a casting surface, the pinholes being suppressed to generate so as to meet a predetermined condition;

a polishing step for reducing a roughness of a polished surface obtained by polishing said casting surface to not more than a predetermined value;

15 a painting step for forming a first resin
coating layer on said polished surface after being
polished; and

a plating step for forming a layer of a metal or a metal compound through a dry-type plating on a surface of said resin coating layer.

2. A surface treatment method for a light-metal casting, as described in claim 1, wherein the predetermined condition of the pinholes generated on said polished surface is that the number and a maximum opening dimension of the pinholes generated in a predetermined area of the polished surface is not more than a predetermined value.

3. A surface treatment method for a light-metal casting, as described in claim 2, characterized in that the number of said pinholes is in the range of 1 to 15 per 100 cm² of said polished surface and said maximum opening dimension is not more than 2 mm.

4. A surface treatment method for a light-metal casting, as described in claim 3, characterized in that the number of said pinholes is in the range of 1 to 10 per 100 cm² of said polished surface, said maximum opening dimension is not more than 2 mm and the number of the pinholes having the maximum opening dimension of 1.0

to 2.0 mm is one or zero.

5. A surface treatment method for a light-metal casting, as described in any one of claims 1 to 4, characterized in that a roughness of said polished surface obtained by said polishing step is 6.3 μm in Rmax.

6. A surface treatment method for a light-metal casting, as described in claims 1 to 5, characterized in that a thickness of said first resin coating layer is not less than 10 μm and not more than 40 μm .

7. A surface treatment method for a light-metal casting, as described in claims 1 to 6, characterized in that a transparent second resin coating layer (a topcoat layer) is formed on said metal or metal compound layer.

8. A surface treatment method for a light-metal casting, as described in claim 7, wherein each of said first and second resin coating layers includes a primer coating layer.

9. A surface treatment method for a light-metal casting, as described in claim 7, wherein a thickness of said transparent second resin coating layer (a topcoat layer) is not less than 20 μm and not more than 50 μm .

10. A surface treatment method for a light-metal casting, as described in claim 1, wherein said polishing step is a barrel finishing process.

11. A surface treatment method for a light-metal casting, as described in claim 1, wherein said plating step for forming a layer of a metal or a metal compound through said dry-type plating is a sputtering process.

12. A surface treatment method for a light-metal casting, as described in claim 1, wherein said casting step includes a pressurizing step for applying, by a pressurizing pin, a pressurizing force to a predetermined portion of the molten metal of said light-metal material filled in a die cavity during a solidification process of said molten metal under high pressure.

13. A surface treatment method for a light-metal casting, as described in claim 1, wherein said casting of said light-metal material is an aluminum wheel.

5 14. A shiny aluminum vehicle wheel, characterized in that the aluminum wheel is cast by a high-pressure casting process, in which a molten metal of an aluminum material filled in a cavity of a die for casting a vehicle wheel is pressurized by an ejection plunger and, in a solidification process of the molten metal, a thick
10 portion of the cavity is pressurized by a pressurizing pin arranged in the die, so that pinholes generated in a polished surface of an aluminum casting after being polished has a dimension of not more than 2.0 mm diameter and has a number not more than 15 per 100 cm² area; and
15 that the aluminum wheel comprises a surface-treated layer wherein the casting surface is barrel-polished to form a polished surface with a roughness Rmax of not more than 1.6 μm, a resin coating layer with a thickness of not less than 10 μm and not more than 40 μm is formed as an
20 undercoat on said polished surface, a dry-type plating layer made of a metal or a metal compound is formed on said resin coating layer and a transparent topcoat layer is formed on said dry-type plating layer so as to provide a design surface.

25 15. A shiny aluminum vehicle wheel as described in claim 14, wherein said aluminum material is aluminum.

16. A shiny aluminum vehicle wheel as described in claim 14, wherein said aluminum material is an aluminum alloy.

004400"004400

In order to remarkably reduce the thickness of a priming resin in the case where a dry-type plating layer is coated on a light-metal casting, such as an aluminum wheel cast body (26), and also to realize a metal gloss superior in design quality, a light-metal material is cast by a high-pressure casting process, in which the molten metal filled in a die cavity (14) is pressurized under a predetermined high pressure by an ejection plunger (16) and, as desired, a predetermined portion of the molten metal is pressurized during the solidification process of the molten metal by a pressurizing pin (22) arranged in the die (12). Then, the casting surface of the cast body of the light-metal material which is cast and formed with the size and number of pinholes on the casting surface of the casting being sufficiently reduced, is subjected to a barrel finishing process, thereafter a resin is coated on the finished surface, and a layer of a metal or a metal compound is formed by a dry-type plating on the resin coating surface, so as to produce a light-metal cast product, such as an aluminum wheel, having a design surface with high shininess.

Fig. 1

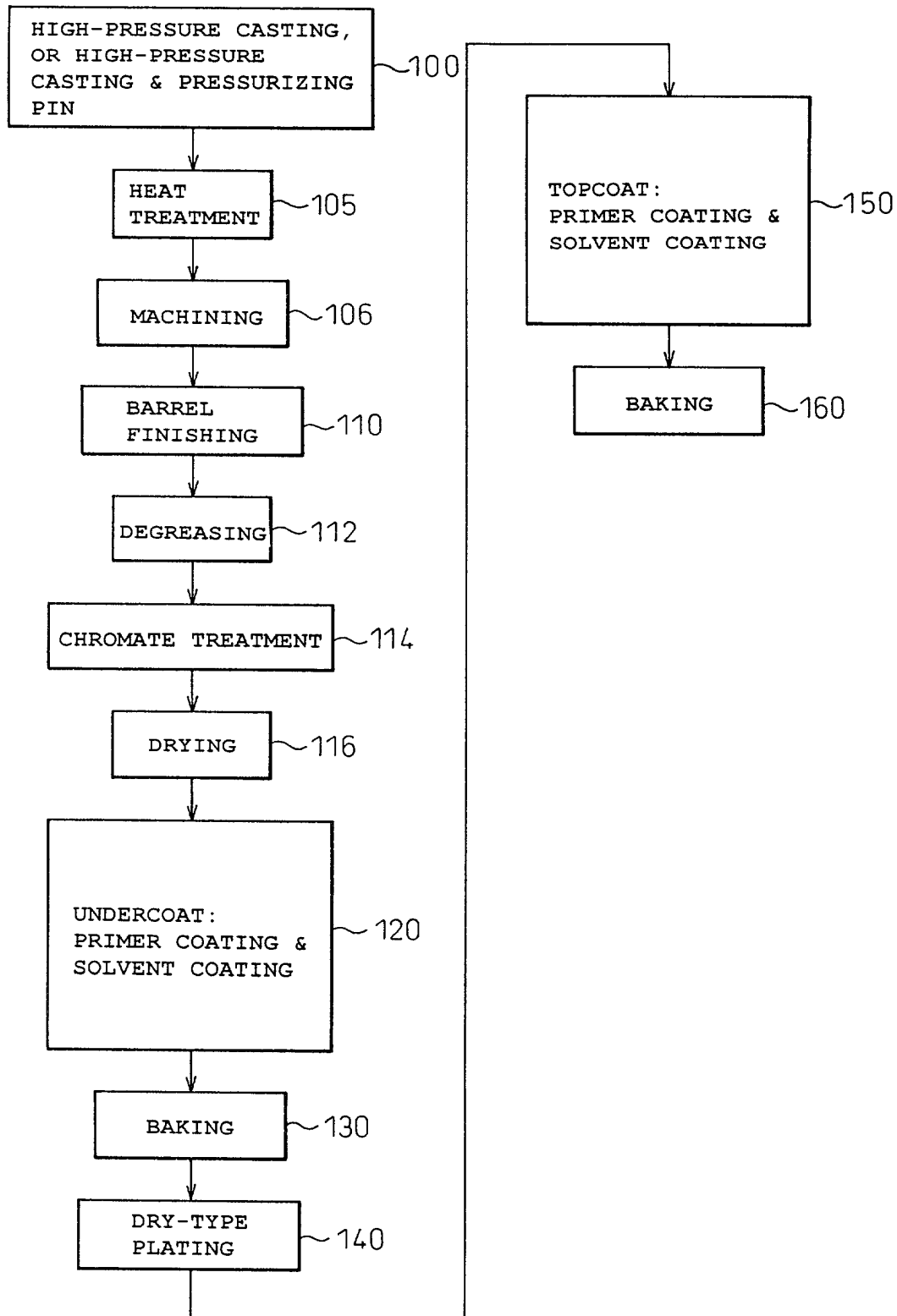


Fig.2

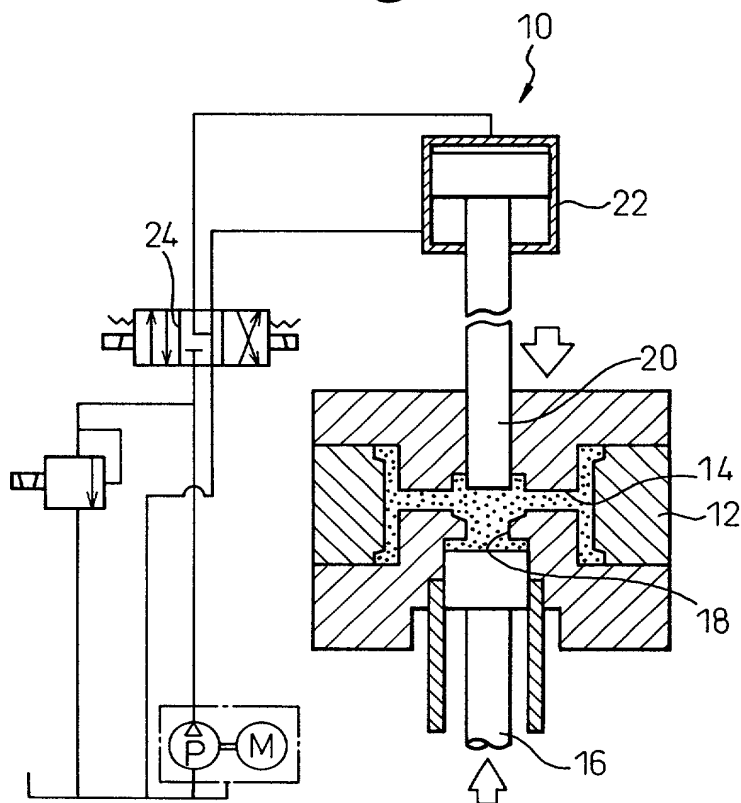


Fig.3

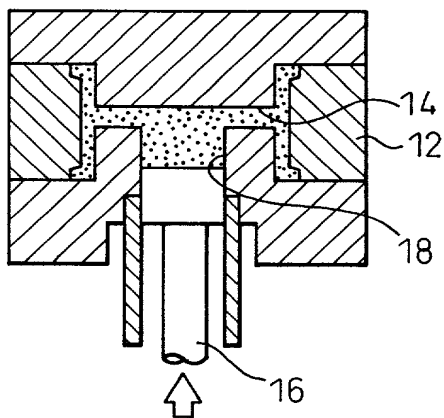


Fig.4

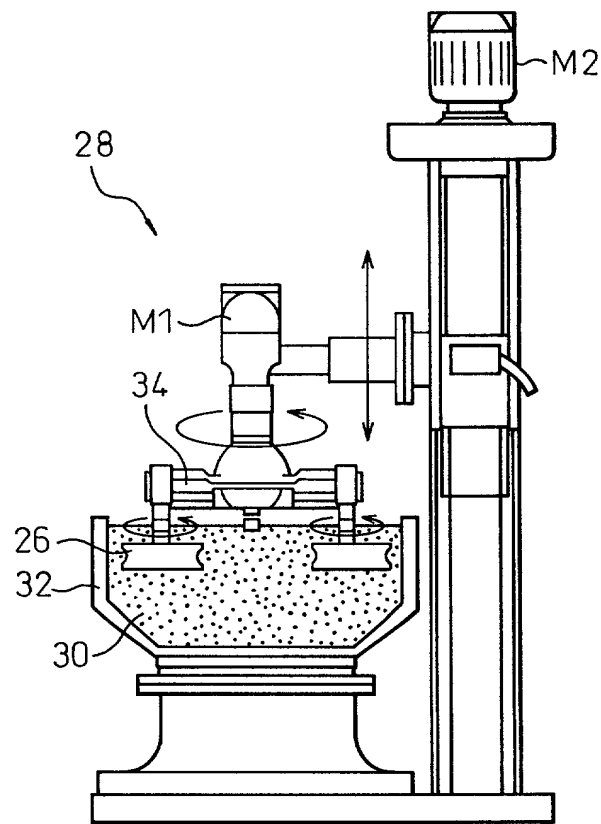


Fig.5

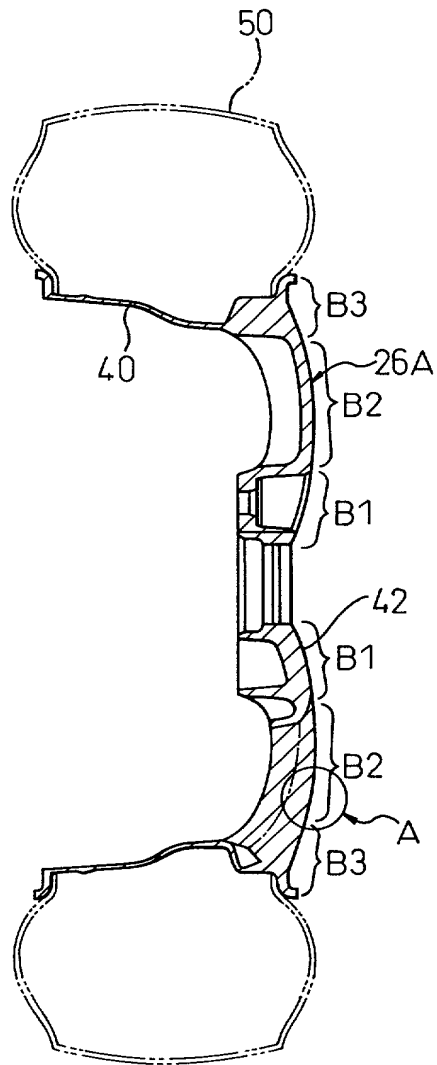
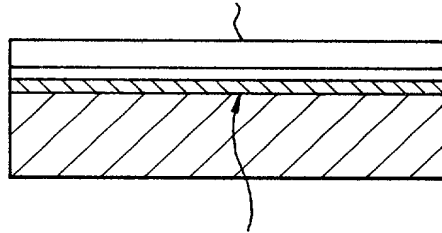


Fig.6A

(INVENTION)

TOPCOAT (25 - 30 μm)

(PRIMER COATING & SOLVENT COATING)



(DRY-TYPE PLATING LAYER)

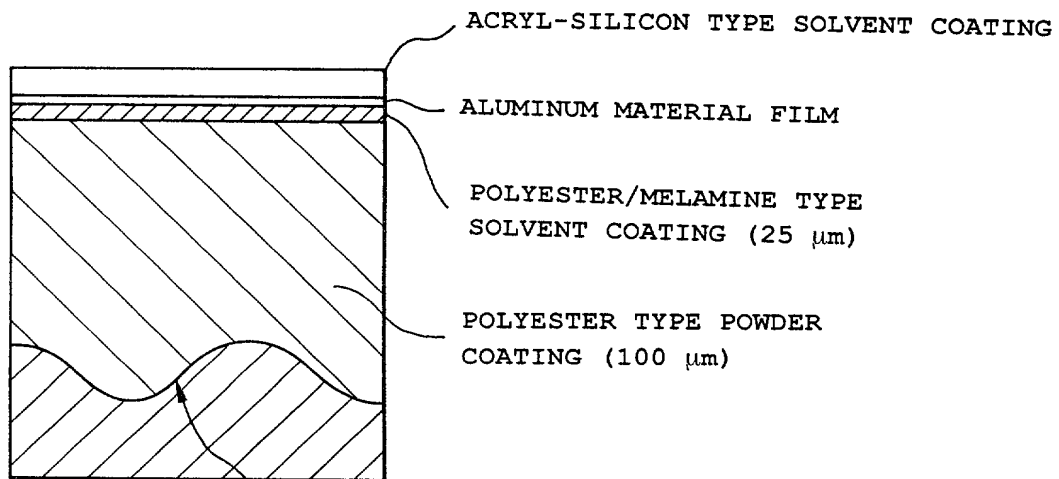
UNDERCOAT (10 - 40 μm)

(PRIMER COATING & SOLVENT COATING)

BUFF FINISHED SURFACE

Fig.6B

(PRIOR ART)



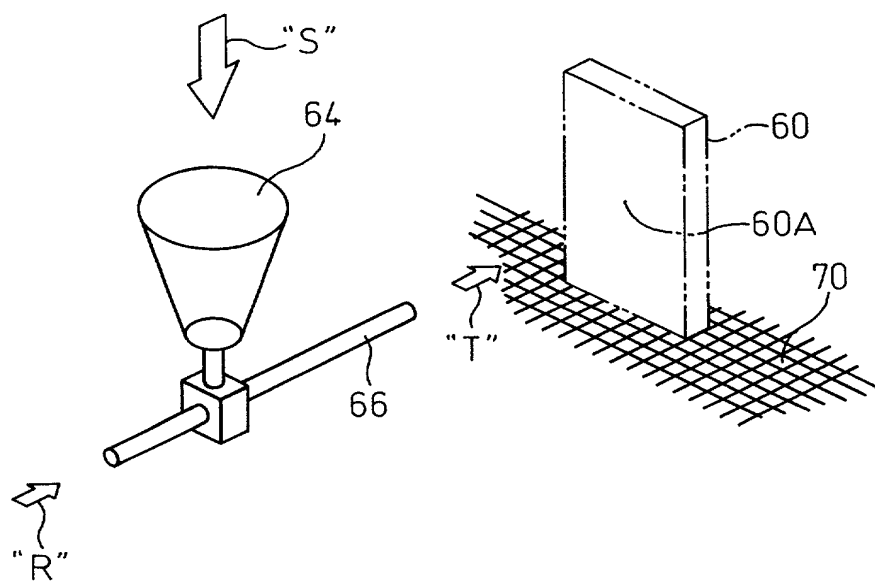
ACRYL-SILICON TYPE SOLVENT COATING

ALUMINUM MATERIAL FILM

POLYESTER/MELAMINE TYPE
SOLVENT COATING (25 μm)POLYESTER TYPE POWDER
COATING (100 μm)

SHOT-BLASTED SURFACE

Fig.7



0000 0000 0000 0000

Fig.8
(PRIOR ART)

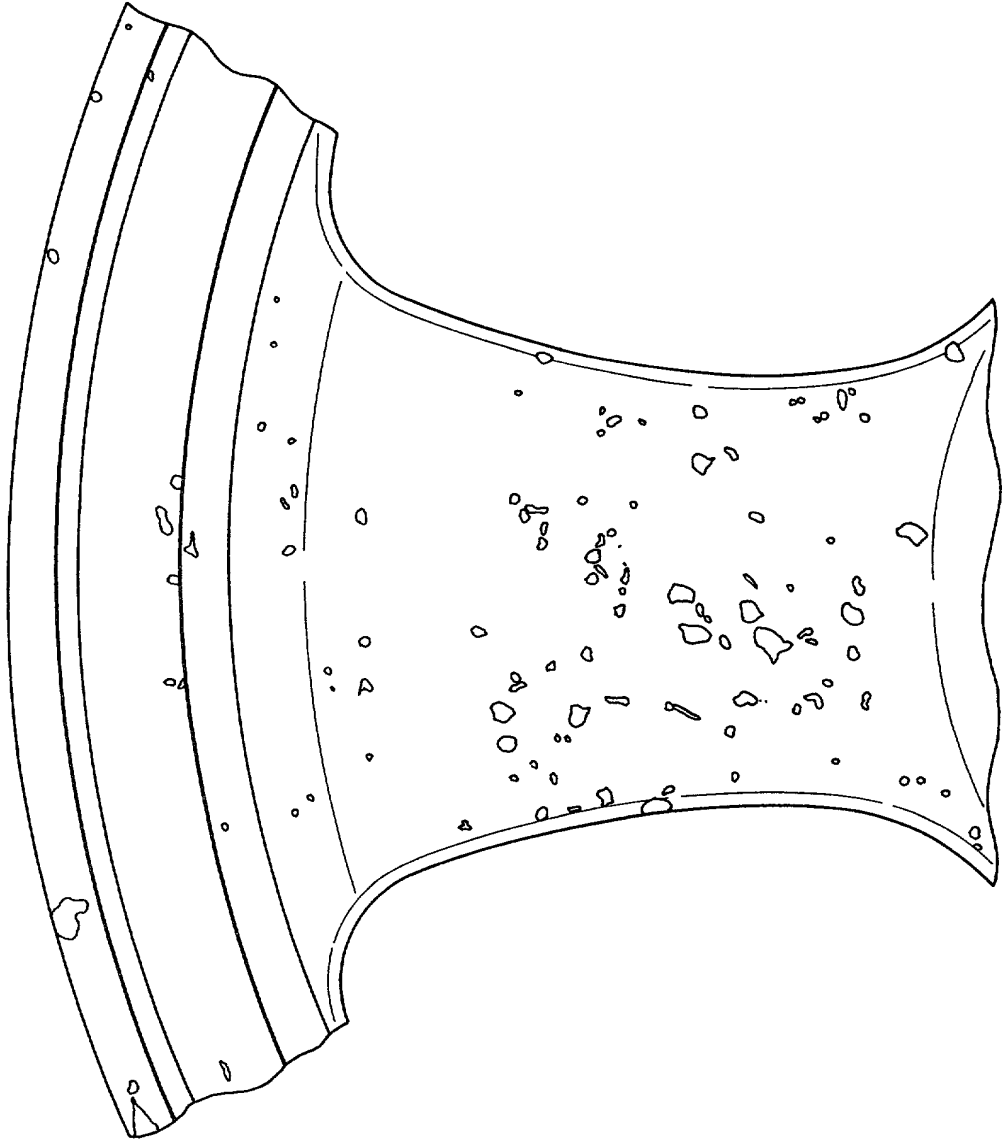
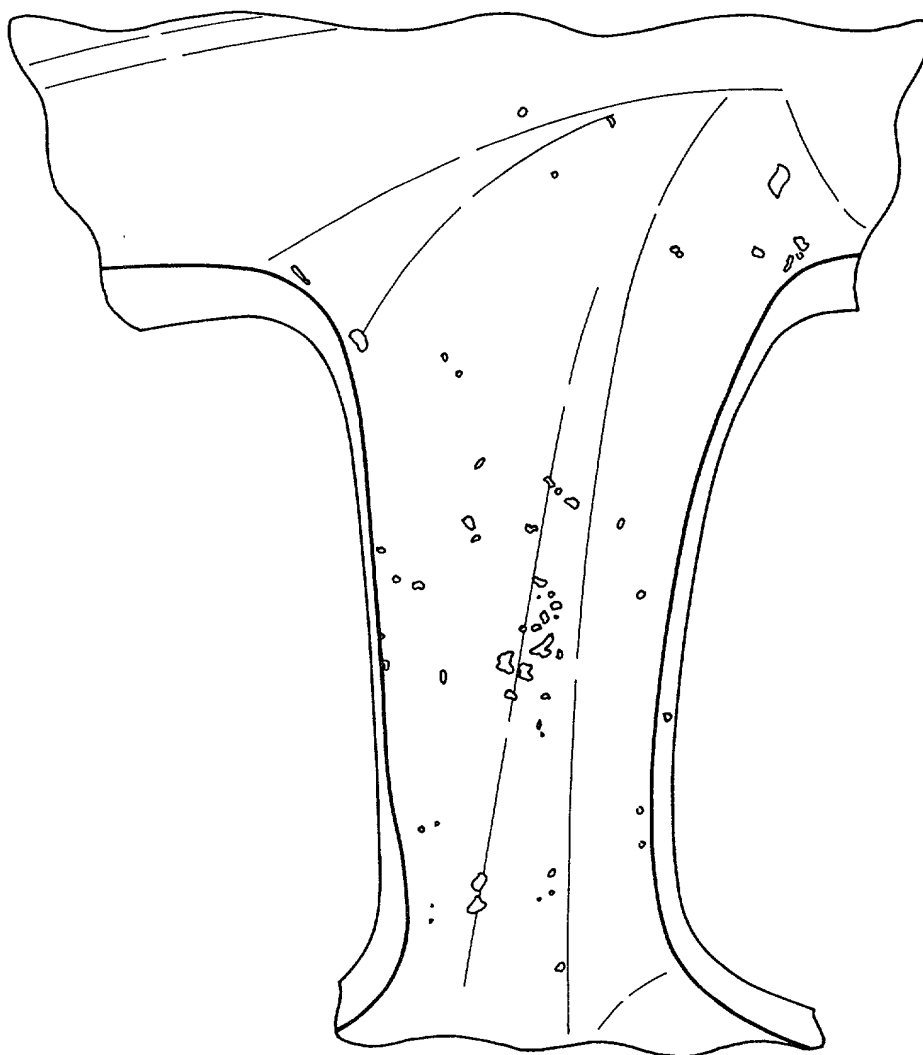


Fig.9

(INVENTION)



LIST OF REFERENCE NUMERALS/ITEMS

10 ... High-pressure casting apparatus
12 ... Die
14 ... Cavity
16 ... Ejection plunger
18 ... Gate
20 ... Pressurizing pin
22 ... Pressurizing cylinder
24 ... Change-over four-way valve
26 ... Aluminum wheel cast body
26a ... Aluminum wheel
28 ... Barrel finishing machine
30 ... Media
32 ... Barrel bath
40 ... Wheel rim
42 ... Wheel hub
50 ... Tire
60 ... Test piece
60A ... Surface to be tested
64 ... Funnel
66 ... Injection pipe
70 ... Screen
M1, M2 ... Motor

Declaration and Power of Attorney For Patent Application

特許出願宣言書及び委任状

Japanese Language Declaration

日本語宣言書

下の氏名の発明者として、私は以下の通り宣言します。

As a below named inventor, I hereby declare that:

私の住所、私書箱、国籍は下記の私の氏名の後に記載された通りです。

My residence, post office address and citizenship are as stated next to my name.

下記の名称の発明に関して請求範囲に記載され、特許出願している発明内容について、私が最初かつ唯一の発明者（下記の氏名が一つの場合）もしくは最初かつ共同発明者であると（下記の名称が複数の場合）信じています。

I believe I am the original, first and sole inventor (if only one name is listed below) or an original, first and joint inventor (if plural names are listed below) of the subject matter which is claimed and for which a patent is sought on the invention entitled

SURFACE TREATMENT METHOD FOR LIGHT-METAL
CAST PRODUCTS AND VEHICLE ALUMINUM WHEEL
TREATED BY THE SAME METHOD

上記発明の明細書（下記の欄でx印がついていない場合は、本書に添付）は、

the specification of which is attached hereto unless the following box is checked:

☐ 月 日 に提出され、米国出願番号または特許協定条約国際出願番号を _____ とし、
（該当する場合） _____ に訂正されました。☐ was filed on January 18, 2000
as United States Application Number or
PCT International Application Number
PCT/JP00/00199 and was amended on _____
(if applicable).

私は、特許請求範囲を含む上記訂正後の明細書を検討し、内容を理解していることをここに表明します。

I hereby state that I have reviewed and understand the contents of the above identified specification, including the claims, as amended by any amendment referred to above.

私は、運邦規則法典第37編第1条56項に定義されたとおり、特許資格の有無について重要な情報を開示する義務があることを認めます。

I acknowledge the duty to disclose information which is material to patentability as defined in Title 37, Code of Federal Regulations, Section 1.56.

Under the Paperwork Reduction Act of 1995, no persons are required to respond to a collection of information unless it displays a valid OMB control number.

Japanese Language Declaration
(日本語宣言書)

私は、米国法典第35編119条(a)-(d)項又は365条(b)項に基づき下記の、米国外の国の少なくとも一カ国を指定している特許協力条約365(a)項に基づく国際出願、又は外国での特許出願もしくは発明者証の出願についての外国優先権をここに主張するとともに、優先権を主張している、本出願の前に出願された特許または発明者証の外国出願を以下に、枠内をマークすることで、示しています。

Prior Foreign Application(s)

外国での先行出願

11-11005(Pat. Appln.)	Japan
(Number)	(Country)
(番号)	(国名)
<hr/>	
(Number)	(Country)
(番号)	(国名)

I hereby claim foreign priority under Title 35, United States Code, Section 119 (a)-(d) or 365(b) of any foreign application(s) for patent or inventor's certificate, or 365(a) of any PCT International application which designated at least one country other than the United States, listed below and have also identified below, by checking the box, any foreign application for patent or inventor's certificate, or PCT International application having a filing date before that of the application on which priority is claimed.

Priority Not Claimed

優先権主張なし

19/January/1999	<input type="checkbox"/>
(Day/Month/Year Filed)	
(出願年月日)	
<hr/>	
(Day/Month/Year Filed)	<input type="checkbox"/>
(出願年月日)	

私は、第35編米国法典119条(e)項に基づいて下記の米国外特許出願規定に記載された権利をここに主張いたします。

(Application No.)	(Filing Date)
(出願番号)	(出願日)

私は、下記の米国法典第35編120条に基づいて下記の米国外特許出願に記載された権利、又は米国を指定している特許協力条約365条(c)に基づき権利をここに主張します。また、本出願の各請求範囲の内容が米国法典第35編112条第1項又は特許協力条約で規定された方法で先行する米国外特許出願に開示されていない限り、その先行米国外出願書提出日以降で本出願書の日本国内または特許協力条約国際提出日までの期間中に入手された、連邦規則法典第37編1条56項で定義された特許資格の有無に関する重要な情報について開示義務があることを認識しています。

(Application No.)	(Filing Date)
(出願番号)	(出願日)

(Application No.)	(Filing Date)
(出願番号)	(出願日)

私は、私自身の知識に基づいて本宣言書中で私が行なう表明が真実であり、かつ私の入手した情報と私の信じることに基づく表明が全て真実であると信じていること、さらに故意になされた虚偽の表明及びそれと同等の行為は米国法典第18編第1001条に基づき、罰金または拘禁、もしくはその両方により処罰されること、そしてそのような故意による虚偽の声明を行なえば、出願した、又は既に許可された特許の有効性が失われることを認識し、よってここに上記のごとく宣誓を致します。

I hereby claim the benefit under Title 35, United States Code, Section 119(e) of any United States provisional application(s) listed below.

(Application No.)	(Filing Date)
(出願番号)	(出願日)

I hereby claim the benefit under Title 35, United States Code, Section 120 of any United States application(s), or 365(c) of any PCT International application designating the United States, listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States or PCT International application in the manner provided by the first paragraph of Title 35, United States Code Section 112, I acknowledge the duty to disclose information which is material to patentability as defined in Title 37, Code of Federal Regulations, Section 1.56 which became available between the filing date of the prior application and the national or PCT International filing date of application.

(Status: Patented, Pending, Abandoned)
(現況: 特許許可済、係属中、放棄済)

(Status: Patented, Pending, Abandoned)
(現況: 特許許可済、係属中、放棄済)

I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

Under the Paperwork Reduction Act of 1995, no persons are required to respond to a collection of information unless it displays a valid OMB control number.

Japanese Language Declaration

(日本語宣言書)

委任状: 私は下記の発明者として、本出願に関する一切の手続きを米特許商標局に対して遂行する弁理士または代理人として、下記の者を指名いたします。(弁理士、または代理人の氏名及び登録番号を明記のこと)

POWER OF ATTORNEY: As a named inventor, I hereby appoint the following attorney(s) and/or agent(s) to prosecute this application and transact all business in the Patent and Trademark Office connected therewith (list name and registration number)

Austin R. Miller, Reg. No. 16,602, T. Daniel Christenbury,

Reg. No. 31,750, David A. Sasso, Reg. No. 43,084,

Patrick J. Farley, Reg. No. 42,524, Joan T. Kluger,

Reg. No. 38,940, James A. Drobile, Reg. No. 19,690,

書類送付先 Sharon Fenick, Reg. No. 45,269, Send Correspondence to:

Michael A. Patane, Reg. No. 42,982, and

Robert A. McKinley, Reg. No. 43,793

IP Department

Schnader Harrison Segal & Lewis, LLP
Suite 3600

1600 Market Street

Philadelphia, PA 19103

直接電話連絡先: (名前及び電話番号)

Direct Telephone Calls to: (name and telephone number)

Austin R. Miller

T. Daniel Christenbury

215-563-1810

唯一または第一発明者名

1-00

Full name of sole or first inventor

Mitsuji Matsui

発明者の署名

日付

Inventor's signature

Date

Mitsuji Matsui

September 11, 2000

住所

Residence

Ube-shi, Yamaguchi, Japan

JP

国籍

Citizenship

Japanese

私書箱

Post Office Address

c/o Ube Machinery and Engineering

Division, Ube Industries, Ltd., 1980,
Aza Okinoyama, Oaza Kogushi, Ube-shi,
Yamaguchi 755-8633, Japan

第二共同発明者

2-00

Full name of second joint inventor, if any

Atsushi Yoshida

第二共同発明者

日付

Second inventor's signature

Date

Atsushi Yoshida

September 11, 2000

住所

Residence

Ube-shi, Yamaguchi, Japan

JP

国籍

Citizenship

Japanese

私書箱

Post Office Address

c/o Ube Machinery and Engineering Division,
Ube Industries, Ltd., 1980, Aza Okinoyama,
Oaza Kogushi, Ube-shi, Yamaguchi 755-8633,
Japan

(第三以降の共同発明者についても同様に記載し、署名をすること)

(Supply similar information and signature for third and subsequent joint inventors.)